## DESIGNING A HYPERBOLIC SECANT EXCITATION PULSE TO REDUCE SIGNAL DROPOUT IN GE-EPI

Stephen James Wastling<sup>1</sup> and Gareth John Barker<sup>1</sup>

<sup>1</sup>Department of Neuroimaging, King's College London, London, United Kingdom

Target audience: This work will be of interest to researchers performing task-based and resting-state FMRI experiments who are investigating regions of the brain currently affected by susceptibility induced signal dropout in gradient-echo echo-planar images.

Purpose: Images acquired using gradient-echo echo-planar imaging (GE-EPI) suffer from signal-dropout in the orbitofrontal cortex (OFC) and temporal lobes (TL) [1]. This artifact can be reduced using RF excitation pulses with quadratic phase profiles [2] such as full-passage scaled-down Hyperbolic Secant (HS) pulses [3-5], which partially cancel the phase dispersion due to susceptibility gradients in the slice-selection direction,  $G_{z,s}$ [2,5]. Here we determine by Bloch simulation the HS pulse parameters needed to give the most uniform signal response across the range of susceptibility gradients observed in the human head ( $G_{z,s} \pm 300 \mu \text{Tm}^{-1}$ ). From these simulations, and from phantom images, we show that previous predictions of the dependence of the voxel signal on the susceptibility gradient [2] are inaccurate. To ensure the slice has the required thickness we derive, for the first time, an expression for the bandwidth,  $\Delta f$ , of a HS pulse used for excitation; this is flip angle dependent, Eq. 1. Finally using our optimised pulse we demonstrate recovery of signal in the orbitofrontal cortex of six healthy male volunteers.

**Theory:** Hyperbolic secant (HS) pulses have both amplitude  $A(t)=A_0\operatorname{sech}(\beta t)$  and phase  $\phi(t)=\mu.\ln[\operatorname{sech}(\beta t)]$  modulation.  $A_0$ , the maximum amplitude of the pulse is related to the desired flip angle,  $\alpha$ , using Eqn. 2.  $\beta$  is the modulation angular frequency; for a fixed pulse duration, T, increasing  $\beta$  reduces the ripple in the stop-band of the slice profile.  $\mu$  is a dimensionless parameter that determines both the sharpness of the slice profile [3] and the degree of quadratic phase [4,5]. It was previously assumed [5] that the bandwidth of an HS excitation pulse was  $\mu\beta/\pi$  (as for inversion [3]), however we show that the bandwidth  $\Delta f$  (FWHM of the transverse magnetisation) is flip angle dependent, Eqn. 1 and Fig. 1.

$$\Delta f = \frac{\beta}{\pi^2} \cosh^{-1} \left[ \frac{\cosh(\pi\mu) (\cos \alpha - 1/2\sqrt{3} + \cos^2 \alpha) + \cos \alpha - 1}{1/2\sqrt{3} + \cos^2 \alpha} - 1 \right]$$
(1) 
$$A_0 = \frac{\beta}{\gamma} \sqrt{ \left( \frac{\cos^{-1} \left[ \cosh^2(\pi\mu/2) \cos \alpha + \sinh^2(\pi\mu/2) \right]}{\pi} \right)^2 + \mu^2}$$
(2)

Methods: An HS pulse was designed such that the signal response for  $G_{z,s} \pm 300 \mu \text{Tm}^{-1}$  was as uniform as possible for 3mm slices acquired with TR=2s and TE=30ms on a 3T GE MR750 system (General Electric, Waukshua, WI, USA) equipped with gradients with max amplitude 50 mTm<sup>-1</sup>. The pulse had T=5ms (to match the SLR pulse excitation pulse being replaced such that the same number of slices could be imaged per TR),  $\alpha$ =73° (Ernst angle for grev-matter at 3T assuming  $T_1=1.6s$  [6]), and  $\beta=3040$ Hz (to minimize the ripple in the slice profile whilst keeping the acoustic noise from gradient switching at an acceptable level). The optimal value of µ was determined by Bloch simulation\* in MATLAB (The MathWorks Inc.). The signal response as a function of  $G_{rs}$  was also measured on the scanner by manually altering the shim gradient prior to acquiring images of a phantom. GE-EPI data with the SLR and the optimal HS pulse were acquired of six healthy male volunteers to determine the degree of signal recovery. Thirty-six slices were acquired top-down sequentially with a 0.3mm slice gaps, with an acceleration (ASSET) factor of two. The field-ofview was 21.2cm with a 64×64 matrix. The body coil was used for RF transmission and an 8-channel head coil was for signal reception. **Results:** The bandwidth, calculated using Eqn. 1 (for  $\mu$ =4.25 and  $\beta$ =3040Hz) is greater than the constant (inversion) bandwidth previously assumed to be valid for all flip angles  $\alpha$ , Fig. 1. Bloch simulation, Fig. 2, shows that the optimal value of  $\mu$ =4.25 results in a signal of ~45-50% (compared to a linear phase pulse when  $G_{z,s}=0$  across  $G_{z,s}\pm 300\mu$ Tm<sup>-1</sup>. In Fig.3 the simulated signal response from a linear phase pulse (red line) is shown along with the simulated (dark blue line) and measured signal response of the HS pulse (green crosses) and the previous theoretical predictions of Cho et al. [2] (light blue line). Previous theoretical predictions [2] do not match simulations and measurements. Relative to a linear phase pulse, signal is recovered when the optimized HS pulse is used for  $G_{z,s}$ <-140 $\mu$ Tm<sup>-1</sup> and >140 $\mu$ Tm<sup>-1</sup>, however the signal is reduced by up to 50% when  $-140\mu$ Tm<sup>-1</sup> < G<sub>z,s</sub><140 $\mu$ Tm<sup>-1</sup>. A representative example from one of the six subjects demonstrates the signal recovery in the OFC when the optimal HS pulse, Fig 4.(b), is used compared to the conventional SLR pulse, Fig 4.(a).





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- Bloch simulation code written by Dr B. Hargreaves (www-mrsrl.stanford.edu/~brian/blochsim)