## Determining Electrical Properties Based on Complex B1-fields Measured in an MR Scanner Using a Multiple Transmit/Receive Coil: a General Approach

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**Introduction** Electrical Property Tomography (EPT) is a recently developed noninvasive technology to measure spatial maps of electrical conductivity and permittivity of biological tissues at radio frequencies used in MR scanners [1]. Because absolute  $B_1$  phase cannot be directly measured in MR experiments [2], current EPT solutions have been proposed based on assumptions about the structure of imaged object and RF coil, phase distribution and main magnetic field, limiting their application to specific scenarios [3–5]. In this study, using a multi-channel transmit/receive coil, we introduce the framework of a new general approach for EPT, which does not depend on previously mentioned assumptions.

**Theory** Inside a piecewise homogeneous medium, based on the principle of reciprocity [6], the superposition of the Cartesian components ( $B_x$  and  $B_y$ ) of  $B_1$  field leads to the Helmholtz equation (1) [7], which associates electrical conductivity  $\sigma$  and relative permittivity  $\varepsilon_r$  with the complex  $B_1$  field  $\tilde{B}_{1j} = |\tilde{B}_{1j}| e^{i\phi_j}$ . Here,  $\tilde{B}_{1j}$  represents either transmit or receive complex  $B_1$  field of channel *j*,  $\phi$  is the absolute phase,  $\omega$  is the Larmor angular frequency, and  $\mu_0$  and  $\varepsilon_0$  are the permeability and permittivity of vacuum,

respectively. Expansion of equation (1) into real and imagery parts and elimination of the

 $\begin{aligned} &-\frac{\nabla^2 \widetilde{B}_{1j}}{\widetilde{B}_{1j} \omega^2 \mu_0} = \varepsilon_r \varepsilon_0 - i \sigma / \omega \quad (1) \\ &\left[ (\frac{\nabla \mid \widetilde{B}_{1j} \mid}{\mid \widetilde{B}_{1j} \mid} - \frac{\nabla \mid \widetilde{B}_{10} \mid}{\mid \widetilde{B}_{10} \mid}) \cdot \nabla \phi_0 = -0.5 \nabla^2 \phi_{rj} - \frac{\nabla \mid \widetilde{B}_{1j} \mid}{\mid \widetilde{B}_{1j} \mid} \cdot \nabla \phi_{rj} \\ &\left[ \nabla \phi_{rj} \cdot \nabla \phi_0 = 0.5 \left( \frac{\nabla^2 \mid \widetilde{B}_{1j} \mid}{\mid \widetilde{B}_{1j} \mid} - \frac{\nabla^2 \mid \widetilde{B}_{10} \mid}{\mid \widetilde{B}_{10} \mid} - \nabla \phi_{rj} \cdot \nabla \phi_{rj} \right) \end{aligned}$ (2)

common terms across channels, such as  $\sigma$  and  $\varepsilon_r$ , will lead to equation (2), where  $|\tilde{B}_{10}|$  and  $\phi_0$  indicate the magnitude and absolute phase of a reference channel, and  $\phi_{rj}$  is the relative phase between channel *j* and the reference channel. Grouping the unknown gradient of absolute phase

 $\nabla \phi_0$  from other measurable components as shown in equation (2),  $\nabla \phi_0$  can be calculated voxel by voxel through solving a linear equation set consisting of multiple channels. Once the absolute phase is obtained,  $\sigma$  and  $\varepsilon_r$  can be calculated based on the Helmholtz equation (1).

<u>Methods</u> A phantom experiment was performed to validate the proposed method. The experiment was carried out in a Siemens MRI system with a 7T Magnet (Magnex Scientific, UK). A single-compartment cylindrical phantom (diameter of 8.7 cm and length of 20 cm) was built using a gel of saline solution, whose  $\sigma$ =0.34 S/m and  $\varepsilon_{r}$ =77 at 298 MHz were measured using a dielectric probe [5]. A 16-channel transceiver RF coil [8] was utilized for both transmission and reception. A hybrid multi-channel  $B_1$  mapping technique [9], [5] using a 3D actual flip angle (AFI) map [10] and a series of 2D gradient-recalled echo (GRE) sequences was used to measure the magnitude and relative phase of receive  $B_1$  fields with a resolution of

1.5x1.5x1.5 mm<sup>3</sup>. Note that this method actually estimates the product of proton density ( $\rho$ ) by receive  $B_1$  fields  $\rho \widetilde{B}_{1j}^-$ ; given the uniform proton

density of the phantom, here  $\rho$  is constant through space. The proton density weighted magnitude of receive  $B_1$  fields  $|\rho \tilde{B}_{1,i}^-|$  and the relative phases

 $\phi_{\vec{r}}$  were used to solve equation set (2). For each channel utilized as a reference, one set of parametric maps of  $\sigma$  and  $\varepsilon_r$  can be calculated using the  $B_1$ 

maps of three other channels. Then sixteen sets of  $\sigma$  and  $\varepsilon_r$  maps (one per channel used as a reference) were combined to form the final solution.

**<u>Results</u>** Shown in figure 1(a) is the relative phase of receive  $B_1$  field measured between channels 4 and 15 in a transverse slice, while figure 1(b) shows the calculated relative phase between the reconstructed absolute phase maps of these two channels using two independent groups of four channels (group 1: channels 4 (reference), 8, 12 and 16;

channels (group 1: channels 4 (reference), 8, 12 and 16, group 2: channels 3, 7, 11 and 15 (reference)). The average difference between the two maps is 0.08 radians and the correlation coefficient (CC) is 97.6%. In the region where the flip angle (FA) used in the AFI sequence was greater than 36° (providing better FA accuracy) over half of the slice, including a central profile (figure. 1(c-d)), the reconstructed  $\sigma$  is 0.33±0.08 S/m and  $\varepsilon$  is 78.2±5.4.

**Discussion and conclusion** In this study we proposed and validated experimentally the framework of a new general approach for solving EPT using measurable components of  $B_1$  fields from multiple channels, which does not depend on assumptions about sample or coil geometry, phase



**Figure 1**. (a)-(b) Measured and estimated relative phase between channel 4 and 15 (c)-(d) Reconstructed profiles of electrical properties across the center of the phantom, red: reconstruction; black: probe measurement.

distribution or field strength. This allows optimized RF excitation strategy of  $B_1$  shimming and channel combination, and RF coil design for improved EPT estimation. This method can be applied at any magnetic field strength and is expected to be especially suitable for fast computation of patient-specific specific absorbing rate (SAR) during an actual scanning session at ultra high field. Different from some other multichannel methods [5], [11], [12], the current approach only requires measuring transmit *or* receive  $B_1$  fields to derive absolute  $B_1$  phases as well as electrical property maps; this can help reducing scanning time and motion induced artifacts for *in vivo* measurement.

**Reference**: [1] Katscher *et al., IEEE Trans Med Imaging* 2009, 28:1365 [2] Van de Moortele *et al., MRM* 2005, 54:1503 [3] Voigt *et al., MRM* 2011, 66:456 [4] van Lier *et al., MRM* 2012 67:552 [5] Zhang et al. *MRM* 2012 (Online) [6] Hoult. *Concepts Magn Reson* 2000, 12: 173 [7] Wen, *Proc. SPIE* 2003, 5030:471 [8] Adriany *et al. MRM* 2008, 59:590 [9] Van de Moortele et al., *ISMRM* 2007, 1676 [10] Yarnykh, *MRM* 2007, 57:192 [11] Katscher *et al., MRM* 2012 (Online) [12] Sodickson et al., *ISMRM* 2012, 387 <u>Acknowledgement</u> NIH R01 EB006433, R01 EB007920, R21 EB014353, T32 EB008389, P41 EB015894, S10 RR26783 and WM KECK Foundation.