Whole-brain and local receive arrays for imaging non-human primates

Kyle M Gilbert¹, Matthew R DiPrimio¹, Sarah Hughes¹, Kathryn Y Manning¹, and Ravi S Menon¹ ¹Robarts Research Institute, The University of Western Ontario, London, Ontario, Canada

Introduction. High-resolution imaging of the cortex in non-human primates (NHP) is limited by the available SNR. To attain high SNR, receive coils must be in close proximity to the brain. In NHP imaging, this is difficult to achieve due to head fixation posts, chambers, and other external hardware attached to the skull. Implanted coil arrays can avoid this problem and significantly increase SNR in NHP imaging (1). A less invasive approach is to create a tight-fitting coil array that can accommodate the external hardware. The purpose of this study was to design a tight-fitting multi-channel receive coil with whole-brain coverage. A secondary, 7-channel receive coil would then be placed inside a recording chamber (used for electrophysiological measurements) to greatly increase SNR over a 5-mm depth in the peripheral visual cortex (see figure 1). The whole-brain receive coil could then be used as an anatomical reference for the location of the smaller chamber coil. The aim is to significantly increase SNR in V1 to be able to discriminate cortical layers (2).

Methods. A 3D anatomical scan was acquired of a cynomolgus monkey. The images were then converted to a 3D former in CAD that could be fabricated using rapid-prototype technology. A 16-channel receive coil was constructed on top of the former, and wire loops Figure 1. A photograph of (a) the transmit coil, (b) were sized and located to avoid external hardware on the skull (i.e., the head post (used for first in derived on the skull (i.e., the head post (used for locations of the head post and chamber are provided by fixation during scanning) and recording chamber could pass through the two different coil the red and black arrows, respectively. elements). The array was then removed from the former, leaving a sparse wire mesh. Coil elements ranged in diameter from 4-5 cm. Loops were constructed from 16-gauge copper wire, with one surface-mount and one variable capacitor for tuning. The coils were connected to low-input-impedance preamplifiers using $n\lambda/2$ cables (~99 cm long; ±5°). Coil matching, active detuning, and preamplifier decoupling were performed on the matching board. A 7channel array, with 6.2-mm-diameter coils, was mounted on the bottom of a 17-mm-diameter Teflon cylinder that could be inserted into the recording chamber of the monkey. Grooves were machined into the Teflon to allow coils to be optimally overlapped and to lay flat on the bottom of the cylinder. Twisted pairs of wire were routed through the cylinder to a tuning capacitor and lattice balun mounted on the opposite end of the cylinder. Lattice baluns were connected to preamplifiers with $n\lambda/2$ cables. No discrete components were located on the coil elements. The transmit coil consisted of two rectangular loops $(16.5 \times 15.2 \text{ cm})$ that were capacitively decoupled. The transmit coil could be placed above the head of the monkey to Figure 2. S12 matrix for the whole-brain coil (ch. 1-16) increase transmit efficiency, or below the head to increase access (at the expense of transmit and chamber coil (ch. 17-23). efficiency).

All performance measurements were acquired on a 7-T human MRI system with a head gradient insert. Signal measurements were recorded using 2D FLASH sequences with both receive coils active. The coils were loaded with a 6.4-cm-diameter phantom filled with 80mM NaCl and 20-mM CuSO₄. Noise correlation was calculated from a noise-only scan with a 1-MHz bandwidth. Whole-brain images were acquired with the 16-channel whole-brain coil while the monkey was positioned headfirst in the sphinx position (TE/TR: 8/1100 ms, matrix: 256×256 , FOV: 9.6×9.6 cm, thickness: 1 mm, N_{slices} : 36, bw: 31 kHz, flip angle: 45°).

Results. The noise correlation of the two coils is shown in figure 2; the noise between the two coil arrays is highly independent. Elements on the whole-brain coil array achieved a minimum and mean S₁₂ of -17 dB and -22 dB, respectively. Preamplifier decoupling increased isolation by 15 dB, and active detuning provided an additional 6 dB during transmission. The chamber coil array achieved S₁₂ values of better than -22 dB, and a 28-dB isolation to the nearest coil element on the whole-brain receive array. Despite the small coil size, preamplifier decoupling was capable of increasing the mean isolation by 13 dB, and active detuning provided an additional 6 dB isolation during transmission.

The 3-8 fold increase in signal was produced by the chamber coil array, over a 5-mm depth in the periphery of the phantom, compared to the whole-brain coil array (figure 3). An anatomical image of an NHP is shown in figure 4. Images show excellent coverage in the visual cortex, despite coils in close proximity to the visual cortex being partially orthogonal to the static field. The coil is able to see the entire brain with uniform contrast.

Conclusions. The utility of employing two separate receive arrays to provide whole-brain coverage of NHPs, while simultaneously significantly increasing SNR in a localized region, is shown. Both coil arrays have the ability to accelerate, creating the potential for highresolution anatomical and functional imaging.

References. [1] Janssens et al. Neuroimage 2012;62:1529-1536. [2] Chen et al. Neuroimage 2012;59:3441-3449.









Figure 3. (a) An image acquired with both the 16channel whole-brain coil and 7-channel chamber coil active. (b) The resultant signal profile.



Figure 4. Four slices of an image acquired with the 16channel whole-brain coil.