Implementation of High-Performance Non-linear O-space Gradient Coil for Accelerated Neuroimaging

Leo K Tam¹, Gigi Galiana², Andrew Dewdney³, William FB Punchard⁴, Kai-ming Lo⁴, Terence W Nixon², John Keiley⁴, Dana C Peters², and R Todd Constable²

¹Biomedical Engineering, Yale University, New Haven, CT, United States, ²Diagnostic Radiology, Yale University, New Haven, CT, United States, ³Siemens AG Healthcare, Erlangen, Bavaria, Germany, ⁴Resonance Research, Inc., Billerica, MA, United States

Target Audience: The gradient hardware, parallel imaging, and non-linear gradient encoding communities. **Introduction**: O-space imaging has demonstrated that non-linear magnetic gradients such as the Z^2 spherical harmonic enable highly accelerated parallel imaging with improved peripheral resolution.¹ Furthermore, PatLoc imaging with orthogonal non-linear gradients suggests that non-linear fields may have lower peripheral nerve stimulation through virtue of a lower dB/dt, and a gradient with the C² and S² spherical harmonics coil was tested.^{2,3} The present work focuses on the design and implementation of a non-linear gradient insert capable of head imaging with high gradient strength and sequence flexibility via integration with the standard gradient amplifiers allowing analogous operation to the traditional linear gradients.

Method: The initial designs for non-linear gradient fields faced an obstacle where the strength and homogeneity of the fields differed from the target field as the measured position moved from isocenter. The non-linear gradient produces concomitant fields of a higher order with the same polarity. The imaging coil can only draw and dissipate a limited amount of power before prohibitive cost and safety limits are reached. This led to an examination of the trade-off between resistive power and homogeneity.

Field Purity Levels within Coil



Fig. 3. Inhomogeneity levels within the 20 cm bore of the gradient insert were suppressed to approximately 10% of the nominal field.



Fig. 1. The O-space approach is a gradient echo projection imaging sequence with three readout channels,

Resistive Power vs. % Inhomogeneity



comes at the cost of increasing power and windings and with diminishing returns.

Reference (top) and Simulated Multi-slice Brain Image at 10% Inhomogeneity (bottom)



Fig. 5. A 128x128x8 numerical phantom reconstructed at $R_z=2$, $R_y=4$ gave accurate reconstructions (MSE =0.0248) with 10% inhomogeneity contingent on incorporation of field deviations into the reconstruction.

For the optimization function, the base strategy was a proprietary version of Powell's method (Resonance Research, Inc. Billerica, MA, USA), an unconstrained conjugate direction minimization.⁴ For the Z^2 winding (fig. 2), independent variables were the location of the coil windings, e.g. (ρ_0, z_{01}), (ρ_0, z_{02}), etc. Once a winding pattern was created, simulations evaluated imaging quality at selected inhomogeneity levels. The coil was integrated with a 3T Trio (Siemens AG, Erlangen, Germany) via a master-slave set of gradient amplifiers and controllers.^{5,6}

Results: The acceptable power gave a 10% inhomogeneity from nominal strength (fig. 3) as it was found that the homogeneity could be increased, but at the expense of a resistive power curve with diminishing returns (fig. 4). Simulations confirmed imaging quality was feasible given precise knowledge of the field deviations from nominal specifications (fig. 5). Imaging with a contrast phantom and a human head (fig. 6) showed successful integration of the new system with existing hardware and software.

Discussion: The present study reports preliminary success in the implementation of a non-linear gradient head insert with requisite field purity. Further investigations seek to utilize the advantages of non-linear encoding for fast neuroimaging, for example using parallel echo planar imaging. **References**: ¹Stockmann et. al. Magn Reson Med. 2010. 64: p. 447-456. ²Hennig, et. al. ISMRM 2007, 453. ³Zaitsev, M. et. al. ISMRM 2012, 2579. ⁴Powell, M. Comp. J. 7: 155-162. ⁵Fontius, U. et. al. ISMRM 2006: 127. ⁶Kim, S-E, et. al. ISMRM 2009, 1372.

Acknowledgements: Special thanks to Peter Brown, Maolin Qiu, and Scott McIntyre. This work was supported by NIH BRP R01 EB012289-01 and a NSF Graduate Research Fellowship.



Fig. 2. A sample diagram of two Z^2 wire winding locations is shown. The locations of the windings were optimized based on resistive power and field inhomogeneity. Large gauge wire (AWG #10) was used instead of copper sheets to deliver power (625 W).

Contrast phantom and *in vivo* images at:



Fig. 6. Contrast phantom and first *in vivo* head images (pair-wise SENSE/O-space, top and bottom respectively) at varying acceleration factors. Images were taken at matrix size = 128×128 (contrast phantom), 256×256 (head). TR=100 ms. TE = 5.5 ms. Hz/px = 390. Num. coils = 8. FOV = 250 mm. Slice thickness = 3 cm. Inhomogeneities in the head images affected Cartesian SENSE more adversely than O-space.