

## Theoretical determination of the dielectric constant for passive RF shimming at high field

M. L. Jayatilake<sup>1,2</sup>, J. Storrs<sup>1,3</sup>, W-J. Chu<sup>1,3</sup>, and J-H. Lee<sup>1,4</sup>

<sup>1</sup>Center for Imaging Research, University of Cincinnati, Cincinnati, OH, United States, <sup>2</sup>Department of Physics, University of Cincinnati, Cincinnati, OH, United States, <sup>3</sup>Department of Psychiatry and Behavioural Neuroscience, University of Cincinnati, Cincinnati, OH, United States, <sup>4</sup>School of Energy, Environmental, Biological, and Medical Engineering, University of Cincinnati, Cincinnati, OH, United States

**Introduction:** Optimal image quality for MRI at high fields requires a homogeneous RF ( $B_1$ ) field among others; however, dielectric properties of the human body result in severe  $B_1$  field inhomogeneity. These are resulted from constructive and destructive RF interactions of complex wave behaviour, which become worse with increasing Larmor frequency. Placement of a shim object with high-dielectric constant adjacent to the body has been proposed as a method for reducing  $B_1$  inhomogeneity by altering wave propagation within the volume of interest [1, 2, 3, and 4]. Selecting the appropriate permittivity and the quantity of material for the correction of  $B_1$  field is essential. While previous work determined primarily empirically the dielectric properties of the shim object, this work introduces a theoretical framework for calculating the requisite dielectric constant of the passive shim material and verifies the accuracy using simulated field maps.

**Theory and Methods:** The human head is approximated by a cylinder with radius  $r_1$  of 20 cm. The head lies inside a TEM coil with inner and outer radii  $r_2$  and  $r_3$  of 28 and 34 cm, respectively. The head and coil are coaxial (Fig. 1). The relative permittivity and conductivity of brain is  $\epsilon_r = 58$  and  $\sigma = 0.3\text{S/m}$ , respectively; and both the brain-to-coil and inner-to-outer coil spaces are filled with air with permittivity  $\epsilon_0$  [2]. It is assumed that  $B_1$  field propagates along the  $B_0$  direction. The general solution of the propagating electromagnetic wave has a unique solution at each region with unknown amplitudes. After applying the boundary conditions to wave solutions in each region, the characteristic equation can be determined [5]. The characteristic equation can further be simplified by substituting the first terms in series expansion of the Bessel function. The simplified characteristic equation is

$$f(k_{\rho 0}, k_{\rho}, k_0, k, k_z) = r_1^2 \cdot k_z^2 \cdot k_{\rho}^2 \cdot (k^2 - k_0^2) \cdot (r_2^2 - r_1^2) \cdot \alpha + k_{\rho}^2 \cdot k_{\rho 0}^2 \cdot (2k^2 \cdot k_{\rho 0}^2 \cdot (r_2^2 - r_1^2) + k_{\rho}^2 \cdot k_0^2 \cdot (r_2^2 + r_1^2)) \cdot (r_1^2 \cdot k_z^2 \cdot k_{\rho}^2 \cdot \alpha' - k_{\rho 0}^2 \cdot \alpha) = 0 \quad (1)$$

Here  $k$ ,  $k_0$ ,  $k_z$  and  $k_{\rho}$  are the brain, air, axial and radial propagation constants respectively. The  $k_z$  and  $k_{\rho}$  characterize the RF field amplitude distribution within the brain, where  $\alpha$  and  $\alpha'$  are given below.

$$\alpha = -2 \cdot (r_1^2 + \pi \cdot r_2) / \pi^2 \cdot r_1 \cdot r_3^3 \cdot k_{\rho 0} \quad (2); \quad \alpha' = -2 \cdot (r_1 + \pi \cdot k_{\rho 0} \cdot r_3^2) / \pi^2 \cdot r_1 \cdot r_2 \cdot r_3^2 \cdot k_{\rho 0} \quad (3)$$

The values of  $k_{\rho}$  and  $k_{\rho 0}$  depend on the dielectric properties within the brain and brain-to-coil region.

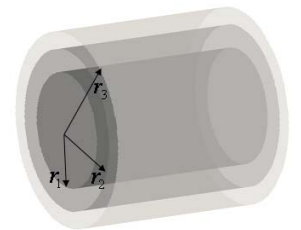
$$k_{\rho}^2 = k^2 - k_z^2 \quad (4); \quad k_{\rho 0}^2 = k_0^2 - k_z^2 \quad (5)$$

Loading with high dielectric material into the brain-to-coil air region significantly influence on the propagation characteristics of the head coil which is demonstrated by changes in  $k_z$ . Combining Eqs. (2), (3), (4) and (5), the  $f(k_{\rho 0}, k_{\rho}, k_0, k, k_z)$  can be expressed as a function of  $k_z$  and  $k_{\rho}$ . The modified characteristic equation can be factored to express the  $k_z$  as a function of the  $k_{\rho}$ . Based on this relationship between radial and axial propagation constants, it is possible to maximize  $k_z$  and minimize  $k_{\rho}$ . Additionally, the  $f(k_{\rho 0}, k_{\rho}, k_0, k, k_z)$  can also be expressed as a function of  $k_z$  and effective dielectric constant ( $\epsilon$ ) in the body-to-coil region, i.e.  $g(k_z, \epsilon)$ . The range of required effective  $\epsilon$  and corresponding  $k_z$  can then be determined when the modified characteristic function  $g(k_z, \epsilon)$  approaches zero. Once the maximal  $k_z$  has been determined, the requisite effective  $\epsilon$  for  $B_1$  passive shimming can be determined.

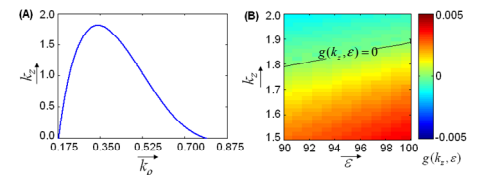
**Results:** Based on the relationship between  $k_{\rho}$  and  $k_z$  (Fig. 2A) the minimum  $k_{\rho}$  of  $0.34\text{cm}^{-1}$  is obtained at the maximum  $k_z$  of  $1.82\text{cm}^{-1}$  for a 4T magnet. Additionally, at the first maximum of  $k_z$ , the radial wave length of  $\lambda_{\rho} = 2\pi / k_{\rho}$  is about  $18.5\text{cm}$  which is comparable to the size of the subject's brain. According to Fig. 2B the appropriate magnitude range of the effective  $\epsilon$  of 92 - 94 is determined corresponding to  $k_z$  of  $1.82\text{cm}^{-1}$  as  $g(k_z, \epsilon)$  reaches zero. Fig. 3 shows the simulated  $B_1$  field map after filling the body-to-coil region with (A) air and (B) a dielectric material with  $\epsilon$  of 94 which is obtained according to Eq. (1). The  $B_1$  field map is normalized to the field amplitude at the center of the FOV with the assumption that the entire brain has a uniform dielectric constant. The results clearly show that the ripples of the  $B_1$  field distribution within the brain are significantly reduced as the  $\epsilon$  within the body-to-coil region increased.

**Discussion:** We have demonstrated with simulation data, as shown in Fig. 3, that this method provides an effective solution for selecting an appropriate material to improve  $B_1$  field homogeneity within the human brain at 4T. This approach should be applicable to all fields. Experimental verification of the method is currently being conducted *in vivo*.

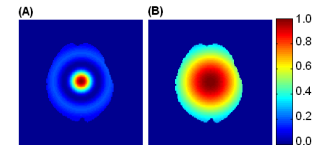
**References:** [1] Haines et al., J Magn Reson Imaging 203;323-327 (2010). [2] Foo et al., Magn Reson Med 23:287- 301(1992). [3] Yang et al., J Magn Reson Imaging 24;197-202(2006). [4] Yang et al., J Magn Reson Imaging 47;982-989(2002). [5] Foo et al., Magn Reson Med 21:165-177(1991).



**Figure 1** Cylindrical model of brain, coil and RF shield.



**Figure 2**(A) Plot of the correlation of axial vs. radial propagation constant. (B) The distribution of the modified characteristic equation of  $g(k_z, \epsilon)$  according to variation of both axial propagation constant and dielectric constant.



**Figure 3** The RF field distributions for axial slices of the subject's brain.