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**INTRODUCTION.** We design & demonstrate a 7-ms slice-selective pulse that mitigates  $B_1^+$  inhomogeneity in the human brain at 7T without the use of a parallel transmission system. At high field, severe RF inhomogeneity due to wavelength interference & attenuation causes standard slice-selective pulses (SSSPs) to produce *non-uniform* flip angles across the field of excitation (FOX), leading to contrast & SNR non-uniformity. One way to mitigate  $B_1^+$  inhomogeneity is to use spoke-based RF pulses; these are comprised of weighted sinc-like segments in  $k_z$  placed at different locations in  $(k_x, k_y)$  that play along an echo-volumnar trajectory [1,2]. In the small-tip-angle regime [3], the sinc segments excite a slice in z, while the  $(k_x, k_y)$  weights tailor the in-plane excitation into the pointwise-inverse of the inhomogeneity. The work here extends our earlier effort [4] to *in vivo* trials & makes use of recent techniques: a magnetization reset pulse to permit fast (TR $\ll$ T<sub>1</sub>) acquisition of multiple images [5], the fitting of these images to an intensity equation to estimate  $B_1^+$ , & a novel sparsity-enforced spoke placement to find a small set of spoke locations & weights [6].

**THEORY & METHODS. Signal intensity equations.** Image intensity  $I_V$  at location  $\mathbf{r}$  due to an SSSP with peak voltage V is:

$$\begin{split} & [I_{V}(\mathbf{r}) = c \cdot \rho(\mathbf{r}) \cdot B_{1}^{-}(\mathbf{r}) \cdot \sin(\alpha_{\circ}(\mathbf{r})) [1 - E_{1}(\mathbf{r}, TR)] [1 - E_{1}(\mathbf{r}, TR) \cos(\alpha_{\circ}(\mathbf{r}))]^{-1}] \text{ (Eq. 1),} \\ & \text{where } c \text{ is a constant, } \rho \text{ proton density, } B_{1}^{-} \text{ the receive profile,} \\ & E_{1}(\mathbf{r}, TR) = \exp(-TR/T_{1}(\mathbf{r})), \text{ and } \alpha_{\circ}(\mathbf{r}) = \gamma V \tau \cdot B_{1}^{+}(\mathbf{r}), \text{ where } \tau \text{ is the SSSP's} \\ & \text{duration } \& B_{1}^{+} \text{ is in Tesla/volt. Let } R(\mathbf{r}) \equiv \rho(\mathbf{r}) \cdot B_{1}^{-}(\mathbf{r}). \text{ With a reset pulse [5],} \\ & \overline{I_{V}(\mathbf{r})} = c \cdot R(\mathbf{r}) \cdot [1 - E_{1}(\mathbf{r}, TR)] \cdot \sin(\alpha_{\circ}(\mathbf{r})) \text{ (Eq. 2), i.e., the } T_{1}\text{-denominator is removed (even if } TR \ll T_{1}). \text{ Finally, if } \alpha_{\circ} \text{ is small and a reset pulse is } \mathbf{not} \text{ used,} \\ & \cos(\alpha_{\circ}) \simeq 1, \sin(\alpha_{\circ}) \simeq \alpha_{\circ}, \text{ and thus } \overline{I_{V}(\mathbf{r})} = c \cdot R(\mathbf{r}) \cdot \alpha_{\circ}(\mathbf{r}) \text{ (Eq. 3).} \end{split}$$

**Profile estimation.** To estimate  $B_1^+(\mathbf{r})$ , we collect N images with increasing V using an SSSP + reset pulse [5]. Then  $\forall \mathbf{r} \in FOX$ , we fit the N values to Eq.2. To estimate  $R(\mathbf{r})$ , we collect a low-flip-angle image,  $L_0(\mathbf{r})$ , without a reset pulse. Eq.3 now holds, and  $L_0(\mathbf{r}) / B_1^+(\mathbf{r})$  yields  $R(\mathbf{r})$  within a constant.

Sparsity-Enforced Spoke Placement (SESP) & pulse design. To minimize pulse duration, only a few spokes may be used; each must be placed & weighted such that the excitation resembles  $[B_1^+(\mathbf{r})]^{-1}$ , so that the overall magnetization  $m(\mathbf{r})$  is uniform. One may use SESP [4,6] to determine good spoke coordinates: First, discretize space at locations  $\mathbf{r}_i$ ,  $i=1...N_s$ . Next, define a set of candidate spoke locations in 2-D k-space,  $\mathbf{k}_i$ ,  $i=1...N_s$ , with weights  $g_i$ . Let  $\mathbf{m} \in \mathcal{C}^{Ns}$  be a vector of  $m(\mathbf{r}_i)$  samples,  $\mathbf{g} \in \mathcal{C}^{Nf}$  a vector of  $g_i s$ ,  $\mathbf{D}$  a diag. matrix of  $B_1^+(\mathbf{r}_i)$  samples, and  $\mathbf{A} \in \mathcal{C}^{Ns \times Nf}$ , where  $\mathbf{A}_{m,n} \propto \exp(\mathrm{j}2\pi\mathbf{r}_m \cdot \mathbf{k}_n)$ ; then,  $\mathbf{m} = \mathbf{D}\mathbf{A}\mathbf{g}$ . Next, define a target magnetization,  $d(\mathbf{r})$ , sample it, and form  $\mathbf{d} \in \mathcal{C}^{Ns}$ . Finally, solve  $\min_{\mathbf{g}} \|\mathbf{d} \cdot \mathbf{D}\mathbf{A}\mathbf{g}\|_2^2 + \lambda \|\mathbf{g}\|_1$  (for fixed  $\lambda$ ): this yields a *sparse*  $\mathbf{g}$ , one with few large weights, revealing a small set of T locations to be traversed by the gradients.

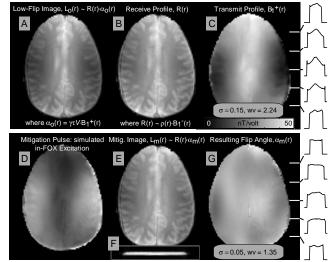
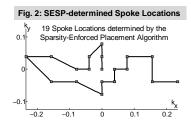


Fig. 1:  $B_1$ + Mitigation Results in the Human Brain at 7T A. Low-flip image,  $L_0(r)$ , collected using standard slice-selective pulse B. Receive profile, R(r), contains proton-density weighting C. *Highly nonuniform* transmit profile,  $B_1$ +(r),  $\sigma$  = 0.15, worst-case variation = 2.24 D.  $B_1$ + Mitigation pulse: simulated in-FOX excitation, strongly resembles [ $B_1$ +(r)]-1 E.  $B_1$ + Mitigation image (in-plane), closely resembles R(r), implying successful mitigation F.  $B_1$ + Mitigation image (through-plane), slice selection is evident G. *Highly uniform* flip angle after mitigation,  $\sigma$  = 0.05, worst-case variation = 1.35

The pulse is designed by fixing spoke shape in  $k_z$ , truncating all but T of  $\mathbf{A}$ 's columns, & retuning the weights by least-squares fitting  $\mathbf{d}=\mathbf{D}\mathbf{A}_{\text{trun}}$ . **Post-mitigation flip angle estimation & quality metrics**.  $B_1^+$  mitigation is quantified by playing the pulse and analyzing the resulting flip angle map,  $\alpha_m(\mathbf{r})$ . This is achieved by obtaining a low-flip mitigation image,  $L_m(\mathbf{r}) \propto R(\mathbf{r}) \cdot \alpha_m(\mathbf{r})$  (per Eq.3). Since  $R(\mathbf{r})$  is known,  $L_m(\mathbf{r})/R(\mathbf{r})$  gives  $\alpha_m(\mathbf{r})$  within a multiplicative constant. The uniformity of  $\alpha_m(\mathbf{r})$  is quantified by computing its in-FOX normalized standard deviation,  $\sigma$ , and worst-case maximum variation, MV (maximum in-FOX value divided by minimum in-FOX value); these values are then compared to those of the initial  $\alpha_0(\mathbf{r})$ .

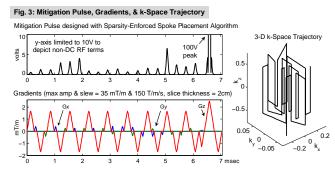


**RESULTS.** Human studies used a 7T scanner, body gradients, and a quadrature birdcage coil in accordance with the institution's HRC. Ten images were collected using SSSPs (V = 20V, 60V, ..., 380V; TR = 1s) followed by resets. Data was fitted to obtain  $\alpha_o(\mathbf{r})$  and  $B_1^+(\mathbf{r})$  (Fig. 1: C); each is highly non-uniform with ( $\sigma$ , MV) = (0.15, 2.24). An  $R(\mathbf{r})$  estimate was obtained from a low-flip SSSP image *without* reset pulse (Fig. 1: A, B).  $B_1^+(\mathbf{r})$  was fed to SESP, and with  $\lambda = 0.35$ , 19 spoke locations were determined (Fig. 2). After fixing spokes to be Hanning-windowed sincs (TBW=4), these locations & weights yielded the 7-ms pulse shown (Fig. 3). This

pulse was simulated (Fig. 1: D) to verify that it yielded approximately  $[B_1^+(\mathbf{r})]^{-1}$ . The pulse was applied *in vivo*, and a low-

flip image obtained (Fig. 1: E); slice selection worked properly (Fig. 1: F). This image was divided by  $R(\mathbf{r})$  to yield  $\alpha_m(\mathbf{r})$  (Fig. 1: G). Qualitatively,  $\alpha_m(\mathbf{r})$  is significantly more uniform than  $\alpha_o(\mathbf{r})$  (compare the 1-D profiles). Quantitatively,  $\sigma$  and worst-case MV have been reduced by factors of 3 and 1.7, respectively, a major flip angle uniformity improvement relative to  $\alpha_o(\mathbf{r})$ .

**CONCLUSION.** *In vivo*  $B_1^+$  inhomogeneity present in the human brain at 7T was mitigated using a 7-ms slice-selective SESP-designed pulse. Commercially-available head-only gradients with amplitude & slew rates of 35 mT/m and 600 T/m/s would allow the use of a 19-spoke, 10-mm excitation pulse that performs  $B_1^+$  mitigation in only 5.25 ms.



**REFERENCES**. [1] Saekho et al. MRM '06;55(4):719-724. [2] Ulloa et al. 2005; ISMRM, p 21. [3] Pauly et al. JMR '89;81:43-56. [4] Setsompop, Zelinski et al. ISMRM '07, p 356. [5] Cunningham et al. MRM '06;55:1326-1333. [6] Zelinski et al. ISMRM '07, p 1691.